YS05S10 DC-DC Converter
3.0-5.5 VDC Input; 0.7525-3.63 VDC Programmable @ 10 A

Bel Power Solutions point-of-load converters are recommended for use with regulated bus converters in an Intermediate Bus Architecture (IBA). The YS05S10 nonisolated DC-DC converter delivers up to 10 A of output current in an industry-standard surface-mount package. Operating from a $3.0-5.5 \mathrm{~V}$ input, the YS05S10 converter is an ideal choice for Intermediate Bus Architectures where Point-of-Load (POL) power delivery is generally a requirement. It provides an extremely tightly-regulated programmable output voltage from 0.7525 V to 3.63 V .
The YS05S10 converter provides exceptional thermal performance, even in high temperature environments with minimal airflow. No derating is required up to 85 C , even without airflow at natural convection. This performance is accomplished through the use of advanced circuitry, packaging, and processing techniques to achieve a design possessing ultra-high efficiency, excellent thermal management, and a very low-body profile.
The low-body profile and the preclusion of heat sinks minimize impedance to system airflow, thus enhancing cooling for both upstream and downstream devices. The use of $100 \%$ automation for assembly, coupled with advanced power electronics and thermal design, results in a product with extremely high reliability.

Applications

- Intermediate Bus Architectures
- Telecommunications
- Data communications
- Distributed Power Architectures
- Servers, Workstations

Benefits

- High efficiency - no heat sink required
- Reduces Total Solution Board Area
- Tape and Reel Packing
- Compatible with Pick \& Place Equipment
- Minimizes Part Numbers in Inventory
- Cost Effective


## 1. ELECTRICAL SPECIFICATIONS

Conditions: $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Airflow $=300 \mathrm{LFM}(1.5 \mathrm{~m} / \mathrm{s})$, Vin $=5 \mathrm{VDC}$, Vout $=0.7525-3.63 \mathrm{~V}$, unless otherwise specified.

| PARAMETER | NOTES | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Absolute Maximum Ratings |  |  |  |  |  |
| Input Voltage | Continuous | -0.3 |  | 6 | VDC |
| Operating Ambient Temperature |  | -40 |  | 85 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature |  | -55 |  | 125 | ${ }^{\circ} \mathrm{C}$ |
| Feature Characteristics |  |  |  |  |  |
| Switching Frequency | Full Temperature Range | 250 | 300 | 350 | kHz |
| Output Voltage Trim Range ${ }^{1,4}$ | By external resistor, See Trim Table 1 | 0.7525 |  | 3.63 | VDC |
| Remote Sense Compensation ${ }^{1}$ | Percent of $\mathrm{Vout}^{(N O M)}$ |  |  | 0.5 | VDC |
| Turn-On Delay Time ${ }^{2}$ | Full resistive load |  |  |  |  |
| With Vin = (Converter Enabled, then Vin applied) | From Vin $=\operatorname{Vin}(\mathrm{min})$ to Vo $=0.1^{*} \mathrm{Vo}$ (nom) | 3 | 3.5 | 4.5 | ms |
| With Enable (Vin = Vin(nom) applied, then enabled) | From enable to $\mathrm{Vo}=0.1^{*} \mathrm{Vo}$ (nom) | 3 | 3.5 | 4.5 | ms |
| Rise time ${ }^{2}$ | From $0.1{ }^{*} \mathrm{Vo}$ (nom) to $0.9 * \mathrm{Vo}$ (nom) | 3 | 3.5 | 5 | ms |
| ON/OFF Control (Positive Logic) ${ }^{3}$ | Converter Off | -5 |  | 0.8 | VDC |
|  | Converter On | 2.4 |  | 5.5 | VDC |
| ON/OFF Control (Negative Logic) ${ }^{3}$ | Converter Off | 2.4 |  | 5.5 | VDC |
|  | Converter On | -5 |  | 0.8 | VDC |
| Input Characteristics |  |  |  |  |  |
| Operating Input Voltage Range |  | 3.0 | 5.0 | 5.5 | VDC |
| Input Undervoltage Lockout |  |  |  |  |  |
| Turn-on Threshold | Guaranteed by controller | 1.95 | 2.05 | 2.15 | VDC |
| Turn-off Threshold | Guaranteed by controller | 1.73 | 1.9 | 2.07 | VDC |
| Maximum Input Current |  |  |  |  |  |
| $\mathrm{V}_{\text {IN }}=4.5 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | $\mathrm{V}_{\text {OUt }}=3.3 \mathrm{VDC}$ |  |  | 7.9 | ADC |
| $\mathrm{V}_{\text {IN }}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | $\mathrm{V}_{\text {Out }}=2.5 \mathrm{VDC}$ |  |  | 9.1 | ADC |
| $\mathrm{V}_{\text {IN }}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | $\mathrm{V}_{\text {Out }}=2.0 \mathrm{VDC}$ |  |  | 7.3 | ADC |
| $\mathrm{V}_{\text {IN }}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | Vout $=1.8 \mathrm{VDC}$ |  |  | 6.7 | ADC |
| $\mathrm{V}_{1 \times}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | Vout $=1.5 \mathrm{VDC}$ |  |  | 5.7 | ADC |
| $\mathrm{V}_{1 \times}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | $\mathrm{V}_{\text {Out }}=1.2 \mathrm{VDC}$ |  |  | 4.7 | ADC |
| $\mathrm{V}_{1 \mathrm{~N}}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | Vout $=1.0 \mathrm{VDC}$ |  |  | 4.0 | ADC |
| $\mathrm{V}_{1 \times}=3.0 \mathrm{VDC}$, lout $=10 \mathrm{~A}$ | Vout $=0.7525 \mathrm{VDC}$ |  |  | 3.2 | ADC |
| Input Stand-by Current (Converter disabled) | $\mathrm{Vin}=5.0 \mathrm{VDC}$ |  | 3.0 |  | mA |
| Input No Load Current (Converter enabled) | Vin = 5.5 VDC |  |  |  |  |
|  | Vout $=3.3 \mathrm{VDC}$ |  | 80 |  | mA |
|  | Vout $=2.5 \mathrm{VDC}$ |  | 80 |  | mA |
|  | Vout $=2.0 \mathrm{VDC}$ |  | 72 |  | mA |
|  | Vout $=1.8 \mathrm{VDC}$ |  | 68 |  | mA |
|  | $\mathrm{V}_{\text {Out }}=1.5 \mathrm{VDC}$ |  | 60 |  | mA |
|  | Vout $=1.2 \mathrm{VDC}$ |  | 55 |  | mA |
|  | $\mathrm{V}_{\text {Out }}=1.0 \mathrm{VDC}$ |  | 50 |  | mA |
|  | Vout $=0.7525$ VDC |  | 42 |  | mA |
| Input Reflected-Ripple Current - is | See Fig. E for setup (BW = 20 MHz ) |  | 10 |  | mAp-p |

+18665132839

| PARAMETER | NOTES | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Output Characteristics |  |  |  |  |  |
| Output Voltage Set Point (no load) |  | -1.5 | Vout | +1.5 | \%Vout |
| Output Regulation ${ }^{4}$ |  |  |  |  |  |
| Over Line | Full resistive load |  | 0.1 | 0.5 | \%Vout |
| Over Load | From no load to full load |  | 0.1 | 0.5 | \%Vout |
| Output Voltage Range | Overall operating input voltage, resistive load and temperature conditions until end of life | -3 |  | +3 | \%Vout |
| Output Ripple and Noise - 20 MHz bandwidth | Over line, load and temperature (Fig. E) |  |  |  |  |
| Peak-to-Peak | $V_{\text {Out }}=3.3 \mathrm{VDC}$ |  | 40 | 60 | $m V_{\text {P-p }}$ |
| Peak-to-Peak | $\mathrm{V}_{\text {out }}=0.7525 \mathrm{VDC}$ |  | 25 | 35 | $m V_{\text {P-P }}$ |
| External Load Capacitance | Plus full load (resistive) |  |  |  |  |
| Min ESR > $1 \mathrm{~m} \Omega$ |  |  |  | 1,000 | $\mu \mathrm{F}$ |
| Min ESR > $10 \mathrm{~m} \Omega$ |  |  |  | 5,000 | $\mu \mathrm{F}$ |
| Output Current Range |  | 0 |  | 10 | A |
| Output Current Limit Inception (lout) |  |  | 18 |  | A |
| Output Short-Circuit Current (Hiccup mode) | Short = $10 \mathrm{~m} \Omega$, continuous |  | 2 |  | Arms |
| Dynamic Response |  |  |  |  |  |
| 50\% Load current change from $5 \mathrm{~A}-10 \mathrm{~A}-5 \mathrm{~A}$ with di/dt=5A/ $\mathrm{s}^{5}$ | $\mathrm{Co}=100 \mu \mathrm{~F}$ tant. $+1 \mu \mathrm{~F}$ ceramic |  | 150 |  | mV |
| Settling Time (Vout < 10\% peak deviation) ${ }^{5}$ |  |  | 60 |  | $\mu \mathrm{s}$ |
| Efficiency | Full load (10 A) |  |  |  |  |
|  | Vout $=3.3$ VDC |  | 94.5 |  | \% |
|  | $\mathrm{V}_{\text {OUt }}=2.5 \mathrm{VDC}$ |  | 93.0 |  | \% |
|  | $V_{\text {out }}=2.0 \mathrm{VDC}$ |  | 92.0 |  | \% |
|  | $\mathrm{V}_{\text {OUt }}=1.8 \mathrm{VDC}$ |  | 91.5 |  | \% |
|  | $V_{\text {Out }}=1.5 \mathrm{VDC}$ |  | 89.5 |  | \% |
|  | $\mathrm{V}_{\text {OUt }}=1.2 \mathrm{VDC}$ |  | 87.5 |  | \% |
|  | Vout $=1.0 \mathrm{VDC}$ |  | 86.0 |  | \% |
|  | Vout $=0.7525 \mathrm{VDC}$ |  | 83.0 |  | \% |

## Notes:

1 The output voltage should not exceed 3.63 V (taking into account both the programming and remote sense compensation).
2 Note that startup time is the sum of turn-on delay time and rise time.
3 The converter is on if ON/OFF pin is left open.
4 Trim resistor connected across the GND (pin 5) and TRIM (pin 3) pins of the converter.
5 See waveforms for dynamic response and settling time for different output voltages.

## 2. OPERATIONS

### 2.1. INPUT AND OUTPUT IMPEDANCE

The YS05S10 converter should be connected via a low impedance to the DC power source. In many applications, the inductance associated with the distribution from the power source to the input of the converter can affect the stability of the converter. The use of decoupling capacitors is recommended in order to ensure stability of the converter and reduce input ripple voltage. Internally, the converter has $44 \mu \mathrm{~F}$ (low ESR ceramics) of input capacitance.
In a typical application, low - ESR tantalum or POS capacitors will be sufficient to provide adequate ripple voltage filtering at the input of the converter. However, very low ESR ceramic capacitors 100-200 $\mu \mathrm{F}$ are recommended at the input of the converter in order to minimize the input ripple voltage. They should be placed as close as possible to the input pins of the converter.
The YS05S10 has been designed for stable operation with or without external capacitance. Low ESR ceramic capacitors placed as close as possible to the load (minimum $100 \mu \mathrm{~F}$ ) are recommended for improved transient performance and lower output voltage ripple.
It is important to keep low resistance and low inductance PCB traces for connecting load to the output pins of the converter in order to maintain good load regulation.

### 2.2. ON/OFF (PIN 1)

The ON/OFF pin is used to turn the power converter on or off remotely via a system signal. There are two remote control options available, positive logic (standard option) and negative logic, with ON/OFF signal referenced to GND. The typical connections are shown in Fig. A.


Fig. A: Circuit configuration for ON/OFF function.

To turn the converter on the ON/OFF pin should be at a logic low or left open, and to turn the converter off the ON/OFF pin should be at a logic high or connected to Vin. See the Electrical Specifications for logic high/low definitions.
The positive logic version turns the converter on when the ON/OFF pin is at a logic high or left open, and turns the converter off when at a logic low or shorted to GND.
The negative logic version turns the converter on when the ON/OFF pin is at logic low or left open, and turns the converter off when the ON/OFF pin is at a logic high or connected to Vin.
The ON/OFF pin is internally pulled up to Vin for positive logic version, and pulled down for a negative logic version. A TTL or CMOS logic gate, open- collector (open-drain) transistor can be used to drive ON/OFF pin. This device must be capable of:

- $\quad$ sinking up to 1.2 mA at a low level voltage of $\leq 0.8 \mathrm{~V}$
- sourcing up to 0.25 mA at a high logic level of $2.3 \mathrm{~V}-5.5 \mathrm{~V}$.

When using open-collector (open-drain) transistor with a negative logic option, add a pull-up resistor ( $\mathrm{R}^{*}$ ) to Vin as shown in Fig. A:

- $\quad 20 \mathrm{~K}$, if the minimum Vin is 4.5 V
- $\quad 10 \mathrm{~K}$, if the minimum Vin is 3.0 V
- $\quad 5 \mathrm{~K}$, if the undervoltage shutdown at $2.05-2.15 \mathrm{~V}$ is required.


### 2.3. REMOTE SENSE (PIN 2)

The remote sense feature of the converter compensates for voltage drops occurring only between Vout pin (Pin 4) of the converter and the load. The SENSE (Pin 2) pin should be connected at the load or at the point where regulation is required (see Fig. B). There is no sense feature on the output GND return pin, where the solid ground plane should provide a low voltage drop.


Fig. B: Remote sense circuit configuration.

If remote sensing is not required, the SENSE pin must be connected to the Vout pin (Pin 4) to ensure the converter will regulate at the specified output voltage. If these connections are not made, the converter will deliver an output voltage that is slightly higher than the specified value.
Because the sense lead carries minimal current, large trace on the end-user board are not required. However, sense trace should be located close to a ground plane to minimize system noise and ensure optimum performance.
When utilizing the remote sense feature, care must be taken not to exceed the maximum allowable output power capability of the converter, which is equal to the product of the nominal output voltage and the allowable output current for the given conditions.
When using remote sense, the output voltage at the converter can be increased up to 0.5 V above the nominal rating in order to maintain the required voltage across the load. Therefore, the designer must, if necessary, decrease the maximum current (originally obtained from the derating curves) by the same percentage to ensure the converter's actual output power remains at or below the maximum allowable output power.

### 2.4. OUTPUT VOLTAGE PROGRAMMING (PIN 3)

The output voltage can be programmed from 0.7525 V to 3.63 V by connecting an external resistor between TRIM pin (Pin 3) and GND pin (Pin 5); see Fig. C. Note that when a trim resistor is not connected, the output voltage of the converter is 0.7525 V .


Fig. C: Configuration for programming output voltage.
A trim resistor, $\mathrm{R}_{\text {tRIm, }}$, for a desired output voltage can be calculated using the following equation:

$$
R_{\text {TRIM }}=\frac{21.07}{\left(V_{\text {OARE }}-0.7525\right)}-5.11 \quad[\mathrm{~K} \Omega]
$$

where,
$\mathbf{R}_{\text {TRIM }}=$ Required value of trim resistor [k K ]
Vorea $=$ Desired (trimmed) output voltage [V]

Note that the tolerance of a trim resistor directly affects the output voltage tolerance. It is recommended to use standard $1 \%$ or $0.5 \%$ resistors; for tighter tolerance, two resistors in parallel are recommended rather than one standard value from Table 1.
Ground pin of the trim resistor should be connected directly to the converter GND pin (Pin 5) with no voltage drop in between. Table 1 provides the trim resistor values for popular output voltages.

| $\mathrm{V}_{\text {O-REG }}$ [V] | Rtrim [k ${ }^{\text {a }}$ ] | The Closest Standard Value [k@] |
| :---: | :---: | :---: |
| 0.7525 | open |  |
| 1.0 | 80.0 | 80.6 |
| 1.2 | 41.97 | 42.2 |
| 1.5 | 23.1 | 23.2 |
| 1.8 | 15 | 15 |
| 2.0 | 11.78 | 11.8 |
| 2.5 | 6.95 | 6.98 |
| 3.3 | 3.16 | 3.16 |
| 3.63 | 2.21 | 2.21 |

Table 1: Trim Resistor Value
The output voltage can also be programmed by external voltage source. To make trimming less sensitive, a series external resistor Rext is recommended between TRIM pin and programming voltage source. Control Voltage can be calculated by the formula:

$$
V_{\text {CTRL }}=0.7-\frac{\left(5.11+R_{\text {Ext }}\right)\left(V_{\text {OREQ }}-0.7525\right)}{30.1} \quad \text { [V] }
$$

where,
VCtrl $=$ Control voltage [V]
$\mathbf{R e x t ~}_{\text {= External }}$ resistor between TRIM pin and voltage source; the value can be chosen depending on the required output voltage range $[\mathrm{k} \Omega$ ].
Control voltages with $\mathbf{R e x t}^{\mathrm{e}}=0$ and $\mathbf{R e x t ~}^{\mathrm{e}}=15 \mathrm{~K}$ are shown in Table 2.

| V0-REG [V] | $\mathrm{V}_{\text {ctrl }}\left(\mathrm{R}_{\mathrm{EXt}}=0\right)$ | $\mathrm{V}_{\text {ctrl }}\left(\mathrm{R}_{\text {ext }}=15 \mathrm{~K}\right)$ |
| :---: | :---: | :---: |
| 0.7525 | 0.700 | 0.700 |
| 1.0 | 0.658 | 0.535 |
| 1.2 | 0.624 | 0.401 |
| 1.5 | 0.573 | 0.201 |
| 1.8 | 0.522 | -0.000 |
| 2.0 | 0.488 | -0.133 |
| 2.5 | 0.403 | -0.468 |
| 3.3 | 0.268 | -1.002 |
| 3.63 | 0.257 | -1.044 |

Table 2: Control Voltage [VDC]

## 3. PROTECTION FEATURES

### 3.1. INPUT UNDERVOLTAGE LOCKOUT

Input undervoltage lockout is standard with this converter. The converter will shut down when the input voltage drops below a pre-determined voltage; it will start automatically when Vin returns to a specified range.
The input voltage must be typically 2.05 V for the converter to turn on. Once the converter has been turned on, it will shut off when the input voltage drops below typically 1.9 V .

### 3.2. OUTPUT OVERCURRENT PROTECTION (OCP)

The converter is protected against overcurrent and short circuit conditions. Upon sensing an overcurrent condition, the converter will enter hiccup mode. Once over-load or short circuit condition is removed, Vout will return to nominal value.

### 3.3. OVERTEMPERATURE PROTECTION (OTP)

The converter will shut down under an overtemperature condition to protect itself from overheating caused by operation outside the thermal derating curves, or operation in abnormal conditions such as system fan failure. After the converter has cooled to a safe operating temperature, it will automatically restart.

### 3.4. SAFETY REQUIREMENTS

The converter meets North American and International safety regulatory requirements per UL/CSA 62368-1 and EN/IEC 62368-1. The maximum DC voltage between any two pins is Vin under all operating conditions. Therefore, the unit has ELV (extra low voltage) output; it meets ES1 requirements under the condition that all input voltages are ELV.
The converter is not internally fused. To comply with safety agencies' requirements, a recognized fuse with a maximum rating of 20 Amps must be used in series with the input line.

## 4. CHARACTERIZATION

### 4.1. GENERAL INFORMATION

The converter has been characterized for many operational aspects, to include thermal derating (maximum load current as a function of ambient temperature and airflow) for vertical and horizontal mountings, efficiency, startup and shutdown parameters, output ripple and noise, transient response to load step-change, overload, and short circuit.
The figures are numbered as Fig. $x . y$, where x indicates the different output voltages, and y associates with specific plots ( $\mathrm{y}=1$ for the vertical thermal derating, ...). For example, Fig. x .1 will refer to the vertical thermal derating for all the output voltages in general.
The following pages contain specific plots or waveforms associated with the converter. Additional comments for specific data are provided below.

### 4.2. TEST CONDITIONS

All data presented were taken with the converter soldered to a test board, specifically a 0.060 " thick printed wiring board (PWB) with four layers. The top and bottom layers were not metalized. The two inner layers, comprised of twoounce copper, were used to provide traces for connectivity to the converter.
The lack of metalization on the outer layers as well as the limited thermal connection ensured that heat transfer from the converter to the PWB was minimized. This provides a worst-case but consistent scenario for thermal derating purposes.

All measurements requiring airflow were made in the vertical and horizontal wind tunnels using Infrared (IR) thermography and thermocouples for thermometry.

Ensuring components on the converter do not exceed their ratings is important to maintaining high reliability. If one anticipates operating the converter at or close to the maximum loads specified in the derating curves, it is prudent to check actual operating temperatures in the application. Thermographic imaging is preferable; if this capability is not available, then thermocouples may be used. . The use of AWG \#40 gauge thermocouple is recommended to ensure measurement accuracy. Careful routing of the thermocouple leads will further minimize measurement error. Refer to Fig. D for the optimum measuring thermocouple location.


Fig. D: Location of the thermocouple for thermal testing.

### 4.3. THERMAL DERATING

Load current vs. ambient temperature and airflow rates are given in Figs. x. 1 and Figs. x. 2 for maximum temperature of $120^{\circ} \mathrm{C}$. Ambient temperature was varied between $25^{\circ} \mathrm{C}$ and $85^{\circ} \mathrm{C}$, with airflow rates from 30 to $500 \mathrm{LFM}(0.15 \mathrm{~m} / \mathrm{s}$ to $2.5 \mathrm{~m} / \mathrm{s}$ ), and vertical and horizontal mountings. The airflow during the testing is parallel to the short axis of the converter, going from pin 1 and pin 6 to pins 2-5.
For each set of conditions, the maximum load current is defined as the lowest of:
(i) The output current at which any MOSFET temperature does not exceed a maximum specified temperature $\left(120^{\circ} \mathrm{C}\right)$ as indicated by the thermographic image, or
(ii) The maximum current rating of the converter (10 A).

During normal operation, derating curves with maximum FET temperature less than or equal to
$120^{\circ} \mathrm{C}$ should not be exceeded. Temperature on the PCB at the thermocouple location shown in Fig. D should not exceed $120^{\circ} \mathrm{C}$ in order to operate inside the derating curves.

### 4.4. EFFICIENCY

Fig. $x .3$ shows the efficiency vs. load current plot for ambient temperature of $25^{\circ} \mathrm{C}$, airflow rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and input voltages of $4.5 \mathrm{~V}, 5.0 \mathrm{~V}$ and 5.5 V . Fig. x .4 is for input voltages of $3.0 \mathrm{~V}, 3.3 \mathrm{~V}$ and 3.6 V and output voltages $\leq 2.5 \mathrm{~V}$.

### 4.5. POWER DISSIPATION

Fig. 3.3V. 4 shows the power dissipation vs. load current plot for $\mathrm{Ta}=25^{\circ} \mathrm{C}$, airflow rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ with vertical mounting and input voltages of $4.5 \mathrm{~V}, 5.0 \mathrm{~V}$ and 5.5 V for 3.3 V output.

### 4.6. RIPPLE AND NOISE

The output voltage ripple waveform is measured at full rated load current. Note that all output voltage waveforms are measured across a $1 \mu \mathrm{~F}$ ceramic capacitor.

The output voltage ripple and input reflected-ripple current waveforms are obtained using the test setup, see Fig. E.


Fig. E: Test setup for measuring input reflected-ripple currents, is and output voltage ripple.


Fig. 3.3V.1: Available load current vs. ambient temperature and airflow rates for Vout $=3.3 \mathrm{~V}$ converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature

$$
\leq 120^{\circ} \mathrm{C} .
$$



Fig. 3.3V.3: Efficiency vs. load current and input voltage for Vout $=3.3$ V converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 3.3V.5: Turn-on transient for Vout $=3.3$ V with the application of Enable signal at full rated load current (resistive) and $100 \mu \mathrm{~F}$ external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage (1 V/div.); Time scale: $2 \mathrm{~ms} /$ div.


Fig. 3.3V.2: Available load current vs. ambient temperature and airflow rates for Vout $=3.3$ V converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 3.3V.4: Power Loss vs. load current and input voltage for Vout $=3.3$ V converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 3.3V.6: Output voltage ripple (20 mV/div.) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5 \mathrm{~V}$ for Vout $=3.3 \mathrm{~V}$. Time scale: $2 \mu s / d i v$.


Fig. 3.3V.7: Output voltage for Vout $=3.3 \mathrm{~V}$ to positive load current step change from 5 A to 10 A with slew rate of $5 \mathrm{~A} \mu \mathrm{~s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage ( $100 \mathrm{mV} / \mathrm{div}$. ); Bottom trace: load current (5 A/div.). Co $=100 \mu$ F ceramic $+1 \mu F$ ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 2.5V.1: Available load current vs. ambient temperature and airflow rates for Vout $=2.5 \mathrm{~V}$ converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 2.5V.3: Efficiency vs. load current and input voltage for Vout $=2.5$ V converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 3.3V.8: Output voltage response for Vout $=3.3 \mathrm{~V}$ to negative load current step change from 10 A to 5 A with slew rate of -5 A $\mu \mathrm{s}$ s at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 $\mathrm{mV} / \mathrm{div}$. ); Bottom trace: load current (5 A/div.). $\mathrm{Co}=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 2.5V.2: Available load current vs. ambient temperature and airflow rates for Vout $=2.5 \mathrm{~V}$ converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 2.5V.4: Efficiency vs. load current and input voltage for Vout $=2.5$ V converter mounted vertically with air flowing at a rate of 200 LFM ( $1 \mathrm{~m} / \mathrm{s}$ ) and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 2.5V.5: Turn-on transient for Vout $=2.5 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu \mathrm{~F}$ external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage (1 V/div.); Time scale: $2 \mathrm{~ms} /$ div.


Fig. 2.5V.7: Output voltage response for Vout $=2.5 \mathrm{~V}$ to positive load current step change from 5 A to 10 A with slew rate of $5 \mathrm{~A} / \mu \mathrm{s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 mV/div.); Bottom trace: load current (5 A/div.). Co $=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu s / d i v$.


Fig. 2.0V.1: Available load current vs. ambient temperature and airflow rates for Vout $=2.0$ V converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 2.5V.6: Output voltage ripple ( $20 \mathrm{mV} /$ div.) at full rated load current into a resistive load with external capacitance $100 \mu \mathrm{~F}$ ceramic $+1 \mu \mathrm{~F}$ ceramic and Vin $=5 \mathrm{~V}$ for Vout $=2.5 \mathrm{~V}$. Time scale: $2 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 2.5V.8: Output voltage response for Vout $=2.5 \mathrm{~V}$ to negative load current step change from 10 A to $5 A$ with slew rate of -5 A/us at Vin $=5 \mathrm{~V}$. Top trace: output voltage $(100$ $\mathrm{mV} / \mathrm{div}$.$) ; Bottom trace: load current (5 A/div.). Co =100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu s / d i v$.


Fig. 2.0V.2: Available load current vs. ambient temperature and airflow rates for Vout $=2.0$ V converter mounted horizontally with Vin = 5 V , and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 2.0V.3: Efficiency vs. load current and input voltage for Vout $=2.0 \mathrm{~V}$ converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 2.0V.5: Turn-on transient for Vout $=2.0 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu$ F external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage ( $500 \mathrm{mV} / \mathrm{div}$. .); Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 2.0V.7: Output voltage response for Vout $=2.0 \mathrm{~V}$ to positive load current step change from 5 A to 10 A with slew rate of $5 \mathrm{~A} \mu \mathrm{~s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage ( 100 $\mathrm{mV} / \mathrm{div}$. .); Bottom trace: load current (5 A/div.). $C o=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 2.0V.4: Efficiency vs. load current and input voltage for Vout $=2.0$ V converter mounted vertically with air flowing at a rate of $200 L F M(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 2.0V.6: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$.) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5 \mathrm{~V}$ for Vout $=2.0 \mathrm{~V}$. Time scale: $2 \mu s / d i v$.


Fig. 2.0V.8: Output voltage response for Vout $=2.0 \mathrm{~V}$ to negative load current step change from 10 A to 5 A with slew rate of $-5 \mathrm{~A} \mu \mathrm{~s}$ s at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 $\mathrm{mV} / \mathrm{div}$. .); Bottom trace: load current ( $5 \mathrm{~A} / \mathrm{div}^{2}$.). Co $=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.8V.1: Available load current vs. ambient temperature and airflow rates for Vout $=1.8 \mathrm{~V}$ converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature

$$
\leq 120^{\circ} \mathrm{C} .
$$



Fig. 1.8V.3: Efficiency vs. load current and input voltage for Vout $=1.8$ V converter mounted vertically with air flowing at a rate of $200 L F M(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.8V.5: Turn-on transient for Vout $=1.8 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu$ F external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage ( $500 \mathrm{mV} / \mathrm{div}$. ); Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 1.8V.2: Available load current vs. ambient temperature and airflow rates for Vout $=1.8 \mathrm{~V}$ converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 1.8V.4: Efficiency vs. load current and input voltage for Vout $=1.8$ V converter mounted vertically with air flowing at a rate of $200 L F M(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.8V.6: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$. ) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5 \mathrm{~V}$ for Vout $=1.8 \mathrm{~V}$. Time scale: $2 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.8V.7: Output voltage response for Vout $=1.8 \mathrm{~V}$ to positive load current step change from 5 A to 10 A with slew rate of $5 \mathrm{~A} / \mu \mathrm{s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 mV/div.); Bottom trace: load current (5 A/div.). Co $=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu s / d i v$.


Fig. 1.5V.1: Available load current vs. ambient temperature and airflow rates for Vout $=1.5 \mathrm{~V}$ converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 1.5V.3: Efficiency vs. load current and input voltage for Vout $=1.5$ V converter mounted vertically with air flowing at a rate of $200 \angle F M(1 \mathrm{~m} / \mathrm{s})$ and $T a=25^{\circ} \mathrm{C}$.


Fig. 1.8V.8: Output voltage response for Vout $=1.8 \mathrm{~V}$ to negative load current step change from 10 A to $5 A$ with slew rate of -5 A $\mu \mathrm{s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage $(100$ $\mathrm{mV} / \mathrm{div}$.$) ; Bottom trace: load current (5 A/div.). C o=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu s / d i v$.


Fig. 1.5V.2: Available load current vs. ambient temperature and airflow rates for Vout $=1.5$ V converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 1.5V.4: Efficiency vs. load current and input voltage for Vout $=1.5 \mathrm{~V}$ converter mounted vertically with air flowing at a rate of $200 \angle F M(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.5V.5: Turn-on transient for Vout $=1.5 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu \mathrm{~F}$ external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage (500 mV/div.); Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 1.5V.7: Output voltage response for Vout $=1.5 \mathrm{~V}$ to positive load current step change from 5 A to 10 A with slew rate of $5 \mathrm{~A} / \mu \mathrm{s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage $(100$ mV/div.); Bottom trace: load current (5 A/div.). Co = $100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.2V.1: Available load current vs. ambient temperature and airflow rates for Vout $=1.2$ V converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 1.5V.6: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$. ) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5$ V for Vout $=1.5$ V. Time scale: $2 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.5V.8: Output voltage response for Vout $=1.5 \mathrm{~V}$ to negative load current step change from 10 A to 5 A with slew rate of $-5 \mathrm{~A} / \mu \mathrm{s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 mV/div.); Bottom trace: load current (5 A/div.). Co = $100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.2V.2: Available load current vs. ambient temperature and airflow rates for Vout $=1.2$ V converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 1.2V.3: Efficiency vs. load current and input voltage for Vout $=1.2 \mathrm{~V}$ converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.2V.5: Turn-on transient for Vout $=1.2 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu$ F external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage ( $500 \mathrm{mV} / \mathrm{div}$.); Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 1.2V.7: Output voltage response for Vout $=1.2 \mathrm{~V}$ to positive load current step change from $5 A$ to $10 A$ with slew rate of $5 \mathrm{~A} \mu \mathrm{~s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage ( 100 $\mathrm{mV} / \mathrm{div}$.); Bottom trace: load current (5 A/div.). Co $=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.2V.4: Efficiency vs. load current and input voltage for Vout $=1.2 \mathrm{~V}$ converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.2V.6: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$.) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5 \mathrm{~V}$ for Vout $=1.2$ V. Time scale: $2 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.2 V.8: Output voltage response for Vout $=1.2 \mathrm{~V}$ to negative load current step change from 10 A to 5 A with slew rate of $-5 \mathrm{~A} \mu \mathrm{~s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 $\mathrm{mV} / \mathrm{div}$. ); Bottom trace: load current ( 5 A div.). $C o=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 1.0V.1: Available load current vs. ambient temperature and airflow rates for Vout $=1.0 \mathrm{~V}$ converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature

$$
\leq 120^{\circ} \mathrm{C} .
$$



Fig. 1.OV.3: Efficiency vs. load current and input voltage for Vout $=1.0$ V converter mounted vertically with air flowing at a rate of $200 L F M(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.0V.5: Turn-on transient for Vout $=1.0 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu$ F external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage ( $500 \mathrm{mV} / \mathrm{div}$. ); Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 1.OV.2: Available load current vs. ambient temperature and airflow rates for Vout $=1.0 \mathrm{~V}$ converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 1.OV.4: Efficiency vs. load current and input voltage for Vout $=1.0$ V converter mounted vertically with air flowing at a rate of $200 L F M(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.0V.6: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$. ) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5 \mathrm{~V}$ for Vout $=1.0$ V. Time scale: $2 \mu s / d i v$.


Fig. 1.0V.7: Output voltage response Vout $=1.0$ V to positive load current step change from 5 A to 10 A with slew rate of 5 A/us at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 mV/div.); Bottom trace: load current (5 A/div.). Co $=100 \mu$ F ceramic + $1 \mu$ F ceramic. Time scale: $20 \mu s / d i v$.


Fig. 0.7525V.1: Available load current vs. ambient temperature and airflow rates for Vout $=0.7525$ V converter mounted vertically with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 0.7525V.3: Efficiency vs. load current and input voltage for Vout $=0.7525$ V converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 1.0V.8: Output voltage response for Vout $=1.0 \mathrm{~V}$ to negative load current step change from 10 A to $5 A$ with slew rate of -5 A/ $\mu$ s at Vin $=5 \mathrm{~V}$. Top trace: output voltage $(100$ $\mathrm{mV} / \mathrm{div}$.$) ; Bottom trace: load current (5 A/div.). C o=100 \mu \mathrm{~F}$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu s / d i v$.


Fig. 0.7525V.2: Available load current vs. ambient temperature and airflow rates for Vout $=0.7525$ V converter mounted horizontally with Vin $=5 \mathrm{~V}$, and maximum MOSFET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 0.7525V.4: Efficiency vs. load current and input voltage for Vout $=0.7525$ V converter mounted vertically with air flowing at a rate of $200 \mathrm{LFM}(1 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 0.7525V.5: Turn-on transient for Vout $=0.7525 \mathrm{~V}$ with the application of Enable signal at full rated load current (resistive) and $100 \mu$ F external capacitance at Vin $=5 \mathrm{~V}$. Top trace: Enable signal (2 V/div.); Bottom trace: output voltage (200 mV/div.); Time scale: 2 ms/div.


Fig. O.7525V.7: Output voltage response for Vout $=0.7525 \mathrm{~V}$ to positive load current step change from 5 A to 10 A with slew rate of $5 \mathrm{~A} / \mathrm{\mu s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage
(100 mV/div.); Bottom trace: load current (5 A/div.). Co = 100 $\mu F$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 0.7525V.6: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$. ) at full rated load current into a resistive load with external capacitance $100 \mu$ F ceramic $+1 \mu$ F ceramic and Vin $=5 \mathrm{~V}$ for Vout $=$ 0.7525 V . Time scale: $2 \mu \mathrm{~s} / \mathrm{div}$.


Fig. O.7525V.8: Output voltage response for Vout $=0.7525 \mathrm{~V}$ to negative load current step change from 10 A to 8 A with slew rate of $-5 \mathrm{~A} / \mu \mathrm{s}$ at Vin $=5 \mathrm{~V}$. Top trace: output voltage (100 mV/div.); Bottom trace: load current (5 A/div.). Co $=100$ $\mu F$ ceramic $+1 \mu$ F ceramic. Time scale: $20 \mu \mathrm{~s} / \mathrm{div}$.

## 5. PHYSICAL INFORMATION



| PAD/PIN CONNECTIONS |  |
| :---: | :---: |
| Pad/Pin \# | Function |
| 1 | ON/OFF |
| 2 | SENSE |
| 3 | TRIM |
| 4 | Vout |
| 5 | GND |
| 6 | Vin |

## YS05S Platform Notes

- All dimensions are in inches [mm]
- Connector Material: Copper
- Connector Finish: Gold over Nickel
- Converter Weight: 0.22 oz [6.12 g]
- Converter Height: 0.327" Max., 0.301" Min.
- Recommended Surface-mount Pads: Min. 0.080 " X $0.112^{\prime \prime}$ [2.03 x 2.84]


## 6. ORDERING INFORMATION

| PRODUC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TSERIES | INPUT |
| VOLTAGE | MOUNTING |
| SCHEME |  |

The example above describes P/N YS05S10-0: 3.0-5.5 V input, surface mount, 10 A at 0.7525 V to 3.63 V output, standard enable logic, and Eutectic Tin/Lead solder. Please consult factory for the complete list of available options.

## For more information on these products consult: tech.support@psbel.com

NUCLEAR AND MEDICAL APPLICATIONS - Products are not designed or intended for use as critical components in life support systems, equipment used in hazardous environments, or nuclear control systems.
TECHNICAL REVISIONS - The appearance of products, including safety agency certifications pictured on labels, may change depending on the date manufactured. Specifications are subject to change without notice.

POWER
SOLUTIONS 8
PROTECTION

